

## STABILISED POWER SUPPLIERS PS2/67, PS2/67A, PS2/67B

**Introduction**

The PS2/67 and its variants each provide supplies from two separate stabilised circuits as shown in Table 1. The units are mounted on chassis CH1/26A, with index pegs in the positions shown.

If this is taken to represent a 24-volt section, the rectifier circuit D1-D4 provides 30 volts d.c. across reservoir capacitor C1 on full load. The series regulator transistor TR6 is fed with a control voltage from the collector circuit of TR5. The

TABLE 1

| Unit    | Output 1 |      | Output 2 |      | Index Pegs |
|---------|----------|------|----------|------|------------|
|         | Volts    | Amps | Volts    | Amps |            |
| PS2/67  | 6        | 1.0  | 24       | 0.5  | 18 42      |
| PS2/67A | 6        | 1.0  | 50       | 0.25 | 24 43      |
| PS2/67B | 12       | 0.75 | 12       | 0.75 | 24 44      |

Output 1 has overvoltage protection which operates at between 7.5 and 8 volts for the PS2/67 and PS2/67A and at between 15 and 16 volts for the PS2/67B. Output 2 of the PS2/67B has overvoltage protection which operates as for output 1.

All outputs have current-limiting circuits of the regenerative type which make the short-circuit current about one-third of the current on full load.

**Circuit Description (Fig. 1)**

The two sections of all three units are similar, except for component values and for the omission of the voltage limiter in the sections providing 24-volt and 50-volt supplies. In the following description component numbers in the upper half of Fig. 1 will be used.

current in this transistor is in turn controlled by the output from a stabilising amplifier TR1, TR2 and TR3, and also by a current overload limiting stage TR4. The control voltage from the stabilising amplifier is the amplified difference between the reference voltage across zener diode D6 and the proportion of the output voltage developed across R10.

The overload transistor TR4 is cut off for all output currents up to the full rated value. As the current through R15 increases above this figure, the base of TR4 becomes negative with respect to its emitter and the transistor conducts. The voltage drop across R2 increases, the collector current of TR5 falls and hence the base current to TR6 falls, thus reducing the current to the load.

The point at which TR4 conducts is set by the adjustment of its base voltage by R12, and the load current drops at this point to a fraction of full load, falling to about a third for a short-circuit load resistance.

If the power supplier is operated near its maximum rated output, care should be taken to avoid the risk of a small increase in load current, which could result in a sudden reduction in the power available from the unit.

The voltage-limiting circuit (if provided) comprises a thyristor CSR2 whose striking voltage is controlled by a zener diode D13. If the output voltage rises above about 7.5 volts (for a nominal 6 volts) or 15 volts (for a nominal 12 volts), the thyristor fires and short-circuits the output. As the shorting current (see *Test Specification*) is limited to 400 mA or less, no damage results even if no action is taken. However, the output voltage

is not restored until the mains input is momentarily disconnected.

### Test Specification

#### Mains Input

Input voltage, 240 volts  $\pm 10$  per cent.

#### Outputs

Test information is given in Table 2.

#### Current Overload Circuit

The current overload circuit should be set to operate at 110 per cent of full load by turning R27 (for output 1) and R12 (for output 2) from its fully clockwise position until the output voltage drops by about 10 per cent from its nominal value when 110 per cent of full load current is drawn.

TABLE 2

| Parameter                               | Output        |              |              |              |
|---|---------------|--------------|--------------|--------------|
|   | 6 Volts       | 12 Volts     | 24 Volts     | 50 Volts     |
| Voltage control                         | R25           | R25 R10      | R10          | R10          |
| Output impedance (d.c.)                 | 0.4 $\Omega$  | 0.6 $\Omega$ | 1.0 $\Omega$ | 2.0 $\Omega$ |
| Output impedance (a.c.) (up to 100 kHz) | 1.2 $\Omega$  | 1.8 $\Omega$ | 3.0 $\Omega$ | 6.0 $\Omega$ |
| Output ripple at full load (p-p)        | < 12 mV       | < 9 mV       | < 6 mV       | < 3 mV       |
| Short-circuit current (mA)              | 300 $\pm 100$ | 250 $\pm 80$ | 130 $\pm 30$ | 80 $\pm 20$  |
| Maximum over-voltage                    | 7.5-8 V       | 15-16 V      | —            | —            |

*Overvoltage Test**(a) Output 1: All Units*

With the outputs open-circuited, connect PLA pin 4 momentarily to the base of TR9. Thyristor CSR1 should fire and the voltage on PLA pins 4 and 5 should be reduced from 6 or 12 volts to  $1.5 \pm 0.5$  volts. Switch off the mains for a few seconds, and on switching on again the normal output voltage should be restored.

Note that, if the negative side of the capacitor C5 is connected by accident to PLA 5, the thyristor will fire and cause fuse FS3 to blow.

*(b) Output 2: PS2/67B Only*

With the outputs open-circuited, connect PLA pin 6 momentarily to the base of TR3. Thyristor CSR2 should fire and the voltage on PLA pins 6 and 7 should be reduced from 12 volts to  $1.5 \pm 0.5$  volts. The normal output voltage can be restored by switching off as before.

If the negative side of C1 is connected by accident to PLA 7, the thyristor will fire and cause FS2 to blow.

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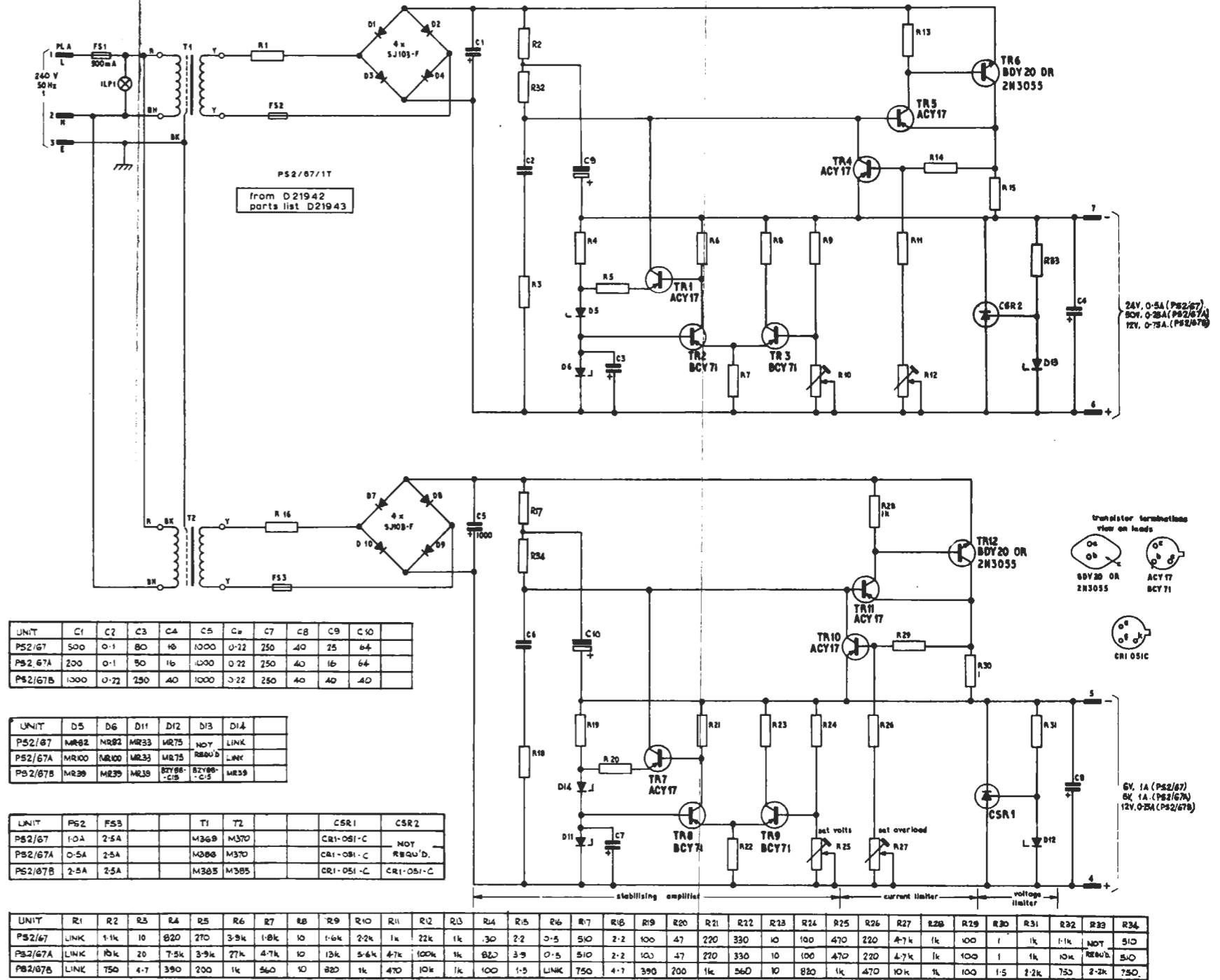


Fig. 1. Circuit of PS2/67 & A & B